

第1章

□ 1

(1)

① $H(s) = \frac{sL}{R+sL}$

② $H(s) = \frac{sCR}{s^2LCR+sL+R}$

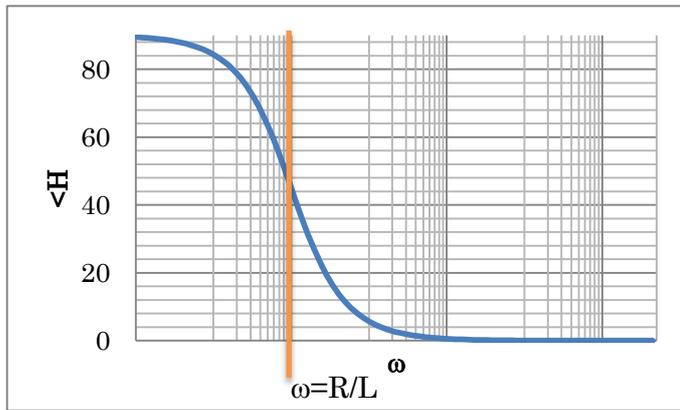
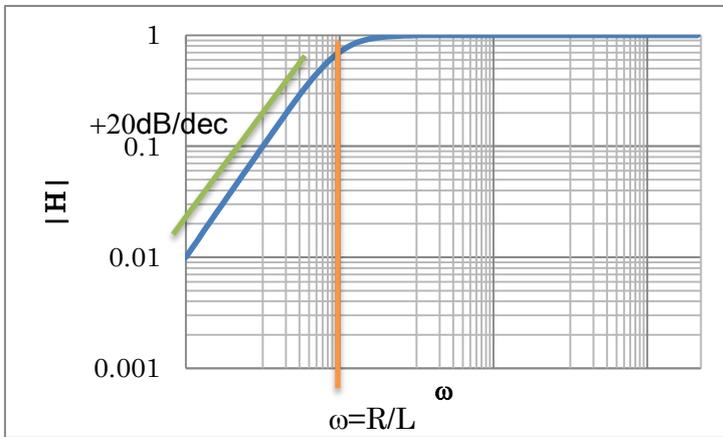
③ $H(s) = \frac{sCR}{s^2CL+sCR+1}$

④ $H(s) = \frac{R}{sL+R}$

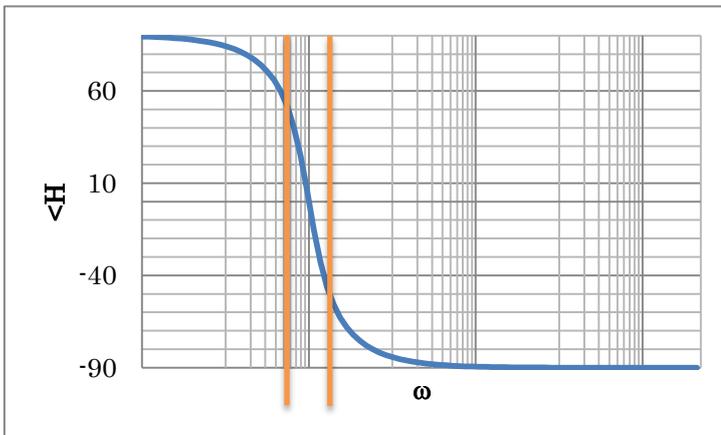
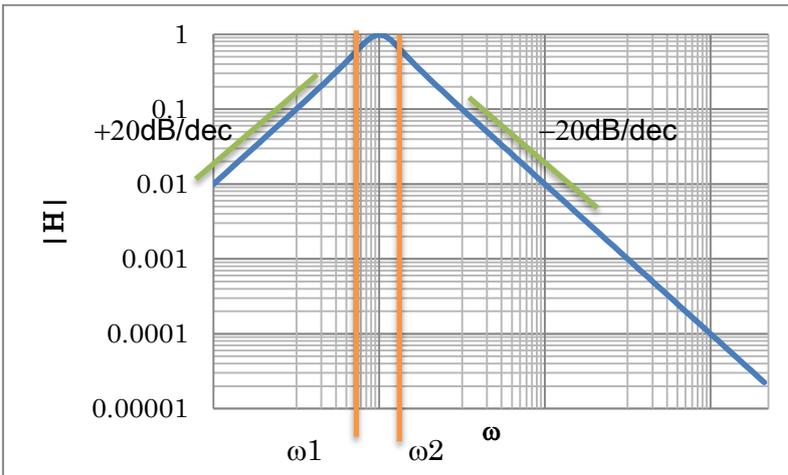
⑤ $H(s) = \frac{s^2CL+1}{s^2CL+sCR+1}$

(2)

①

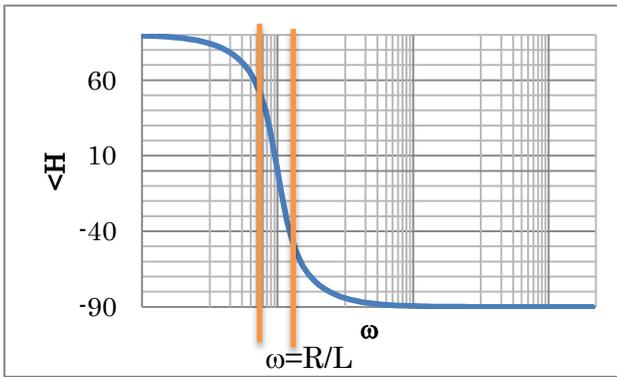
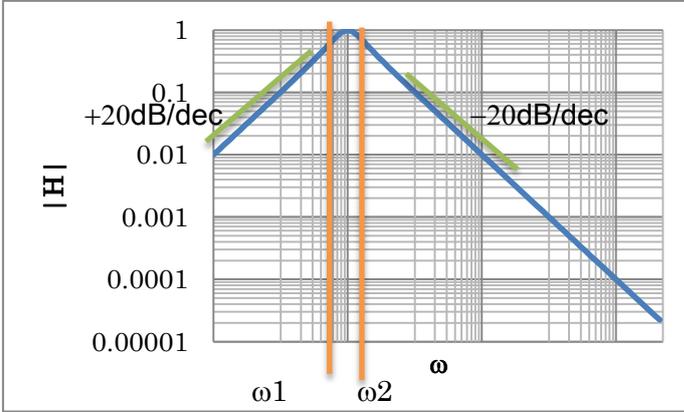


②



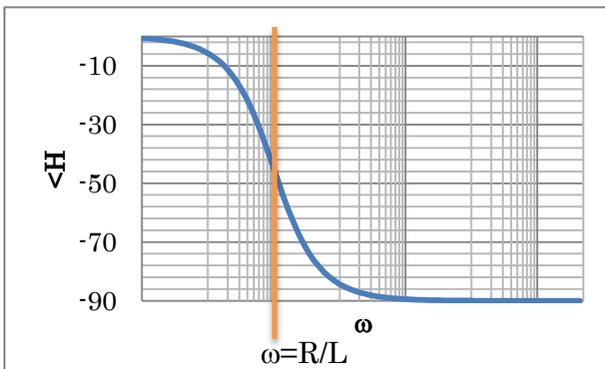
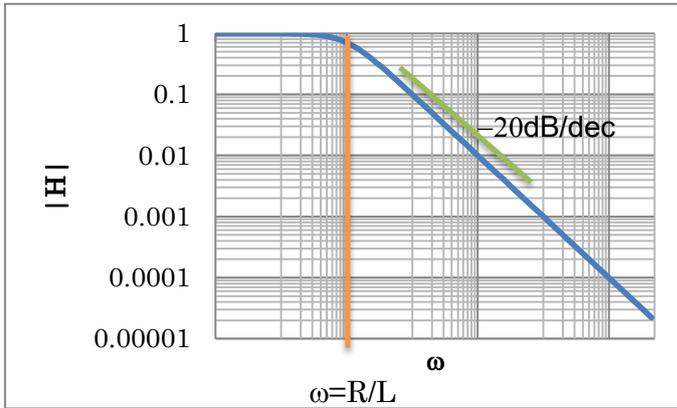
$$\omega_1, \omega_2 = \sqrt{\frac{2CR^2 + L \pm \sqrt{L^2 + 4LCR^2}}{2LC^2R^2}}$$

③

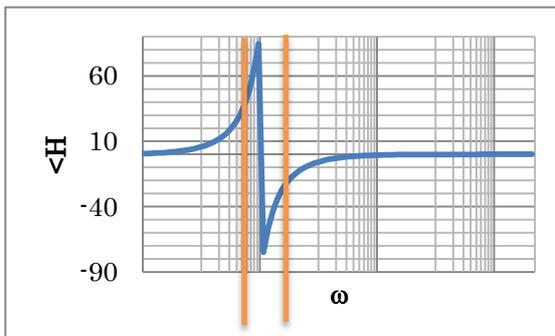
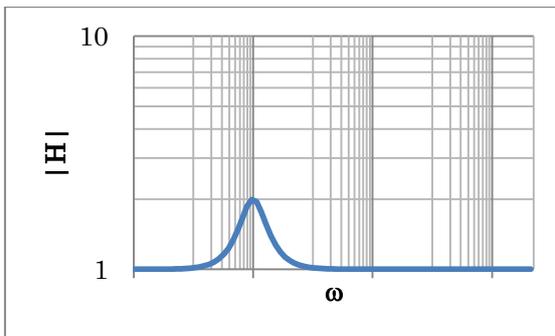


$$\omega_1, \omega_2 = \sqrt{\frac{2L + CR^2 \pm \sqrt{C^2R^2 + 4CL}}{2CL^2}}$$

④



⑤



$$\omega_1, \omega_2 = \sqrt{\frac{2L + CR^2 \pm \sqrt{C^2R^2 + 4CL}}{2CL^2}}$$

(3)

省略

第2章

□ 1

$$(1) C_{ox} = \epsilon \epsilon_r \frac{1}{d} = 4.0 \times 10^{-3} \text{ F/m}^2$$

$$(2) \mu C_{ox} \frac{W}{L} = 350 \times 10^{-4} \times 4 \times 10^{-3} \times \frac{50}{0.5} = 1.4 \times 10^{-2} \rightarrow$$

$$I_d = \frac{1}{2} \mu C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS}) = \frac{1}{2} \times 1.4 \times 10^{-2} \times (5 - 0.7)^2 (1 + 0.5) = 1.9 \times 10^{-1} \\ = 190 \text{ mA}$$

$$(3) g_m = \frac{2I_D}{V_{GS} - V_{TH}} = 10 \text{ mS}$$

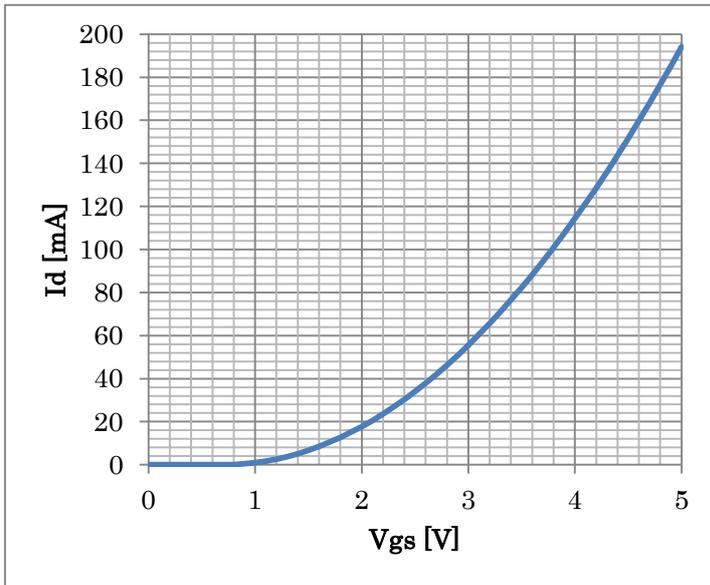
$$\frac{W}{L}: \lambda = 0 \text{ の時} : \frac{W}{L} = \frac{2I_D}{\mu C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2} = 0.357 \approx 0.36$$

実際には $\frac{W}{L} = \frac{2I_D}{\mu C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})}$ である。したがって、

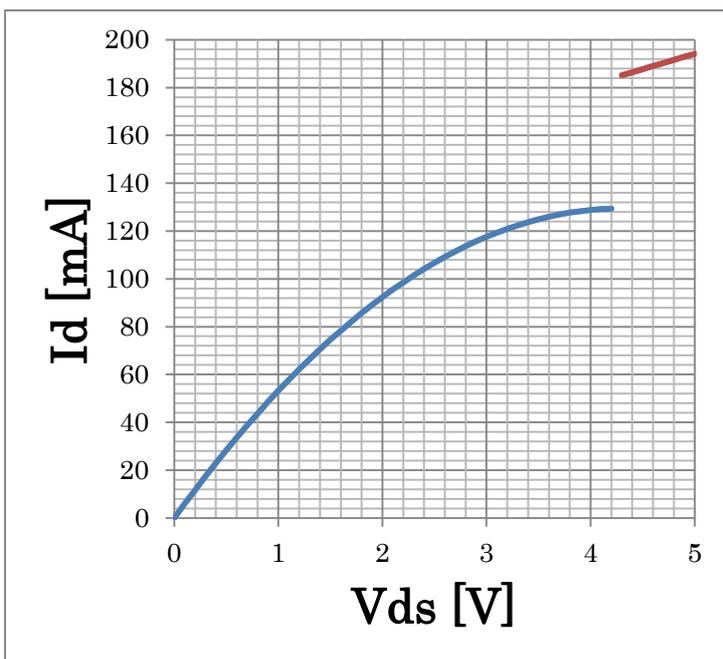
$V_{DS} [\text{V}]$	$\frac{W}{L}$
1	0.32
2	0.30
3	0.27
4	0.26
5	0.24

のようになる。

(4)



(5) 線形と飽和領域でチャネル長変調効果の分段差が生じてしまう



(6) の時トランジスタは飽和領域であるため ($V_{GS} = V_{DS} + V_{TH} = 3.7V$ とした時のドレイン電流が $0.5mA$ より大きくなるため、ゲート電圧が、 $V_{GS} < V_{DS} + V_{TH}$ を満たすため)。

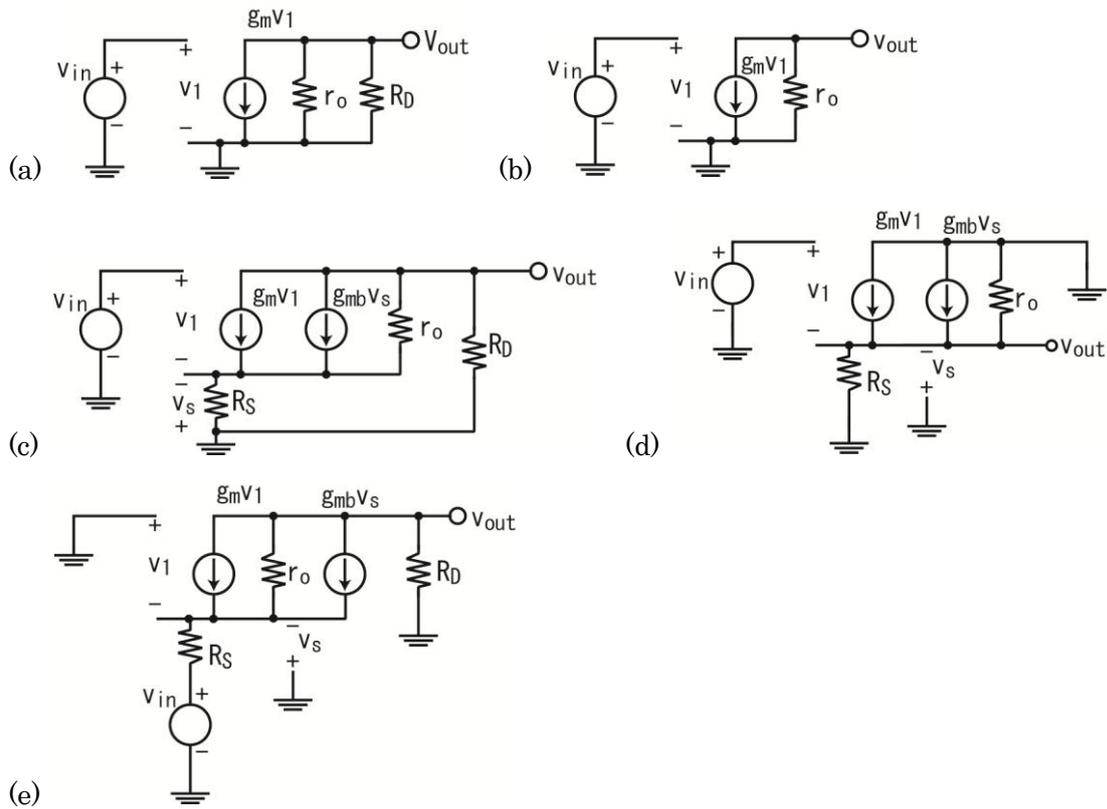
$$\text{よって } (V_{GS} - V_{TH})^2 = \frac{2I_D}{\mu C_{ox} \frac{W}{L} (1 + \lambda V_{DS})} = 0.0549 \rightarrow V_{GS} = V_{TH} + 0.23 = 0.93V$$

$$g_m = \frac{2I_D}{V_{GS} - V_{TH}} = 4.26mS \approx 4.3mS$$

□ 2 この時トランジスタは飽和領域であるため、 $I_d = \frac{1}{2} \mu C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS}) = \frac{1}{2} 10m(3 - 0.7)^2 (1 + 0.1 \times 5) = 39.6mA \approx 40mA$

第3章

□ 1



□ 2 $\Delta I_d = g_m \Delta V_{GS} = 10mS \times 100mV = 1mA$

□ 3

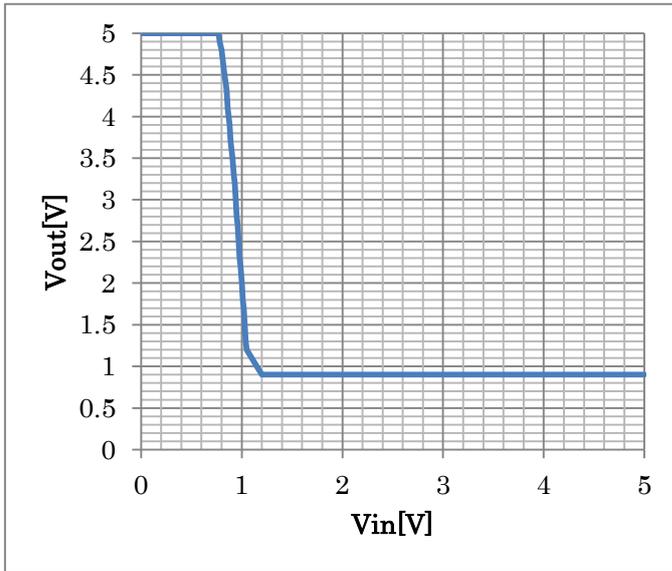
N1: $2C_d + 2C_g$, N2: $2C_d + C_L$

N3: $C_d + C_s$, N4: $2C_d + 2C_g$, N5: $C_d + C_s + 2C_g$, N6: $C_d + C_s$, N7: $2C_d + C_L$, N8: $C_d + C_s$

N9: $C_d + C_s$, N10: $2C_d + C_s$, N11: $C_d + C_s$

第4章

□ 1



□ 2 グラフから読み取る

$$A_v = -20$$

□ 3

(1)、(2)

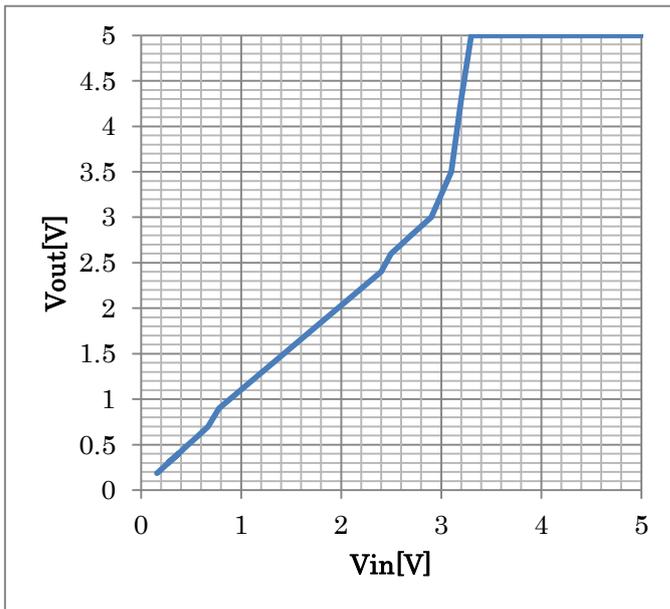
$$(a) A_v = -g_m(r_o || R_D) = -10m(5k || 10k) = -3.3$$

$$(b) A_v = -g_m r_o = -10m \cdot 10k = 100$$

$$(c) A_v = -\frac{g_m r_o R_D}{R_D + r_o + R_S \{1 + (g_m + g_{mb}) r_o\}} = -\frac{10m \cdot 10k \cdot 5k}{10k + 5k + 1k \{1 + (10m + 1m) 10k\}} = -\frac{500}{126} = -3.968 \approx 4.0$$

第5章

□ 1



□ 2 Vin=2V 付近ではトランジスタが線形領域である
 $A_v = 1.0$

□ 3
 (1)、(2)

(d) $A_v = \frac{R_S g_m r_o}{r_o + \{1 + (g_m + g_{mb})r_o\}R_S} = \frac{1k \cdot 10m \cdot 10k}{10k + \{1 + (10m + 1m)10k\}1k} = \frac{100}{121} = 0.826 \approx 0.83$

(e) $A_v = \frac{1 + (g_m + g_{mb})r_o}{R_D + r_o + \{1 + (g_m + g_{mb})r_o\}R_S} R_D = \frac{1 + (10m + 1m)10k}{5k + 10k + \{1 + (10m + 1m)10k\}1k} 5k = \frac{555}{126} \approx 4.4$

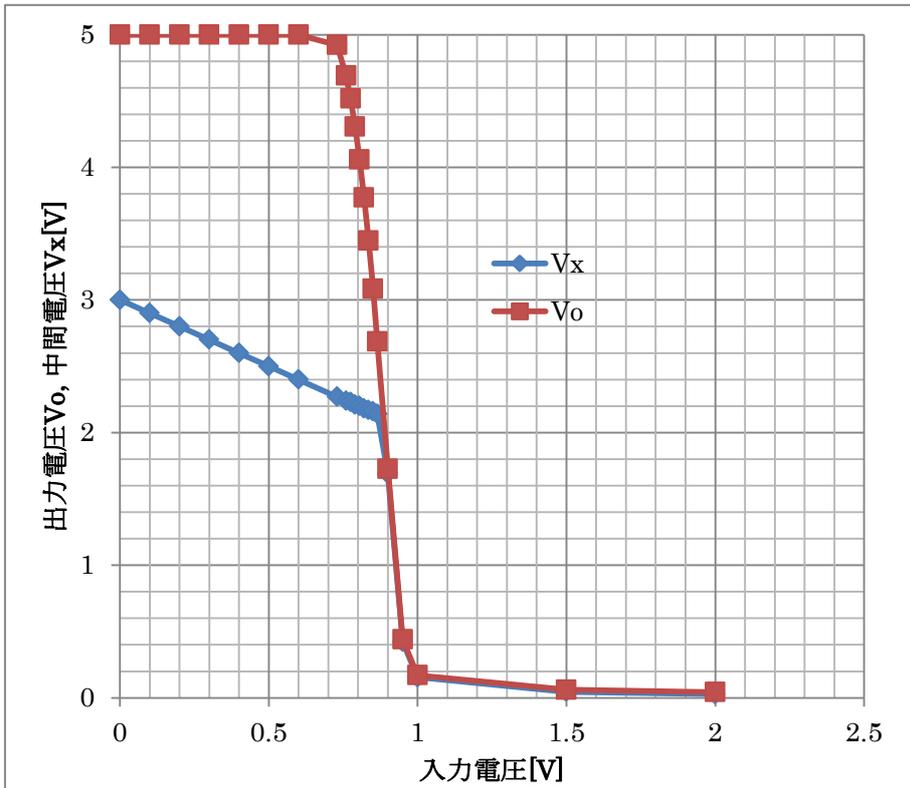
□ 4 $R_{in} = \frac{R_D + r_o}{1 + (g_m + g_{mb})r_o} = 108.9\Omega \approx 110\Omega$

□ 5 $R_{out} = \{1 + (g_m + g_{mb})r_o\}R_S || R_D \approx 94\Omega$

□ 6 $A_v = \frac{R_S g_m r_o}{r_o + \{1 + (g_m + g_{mb})r_o\}R_S} \approx 0.83$

第 6 章

□ 1



□ 2

- (1) $R_{out} = g_m r_o^2 = 1\text{M}\Omega$
- (2) $|A_v| = R_D g_m = 100$
- (3) $A_v = (g_m r_o)^2 = 10,000$

□ 3 $A_v = (g_m r_o)^3 = 1,000,000$

第7章

□ 1

- (1) $A_{v,diff} = \frac{1}{2} g_m R_D = \underline{10}$
- (2) 題意より $g_m R_{SS} \gg 1$ であるため、 $A_{v,com} = \frac{R_D}{2R_{SS}} = \underline{0.01}$
- (3) $CMRR = \frac{A_{v,diff}}{A_{v,com}} = \underline{1000}$

第8章

□ 1

- (1) $R_{out} = \frac{1}{2} r_o = \underline{5\text{k}\Omega}$
- (2) $A_{v,diff} = g_m R_{out} = \frac{1}{2} g_m r_o = \underline{50}$

$$(3) A_{v,com} \approx \frac{1}{1+2g_m R_{SS}} = \underline{0.0005}$$

$$(4) CMRR = \frac{A_{v,diff}}{A_{v,com}} = \underline{100.000}$$

□ 2

$$(1) R_{M3} = \frac{1}{g_{mp} + \frac{1}{r_{op}}} \approx \frac{1}{g_{mp}}$$

$$(2) R_{out} = r_{op} || r_{on}$$

$$(3) v_{out} = -R_{out} \cdot i_{M2} = -g_{mn}(r_{op} || r_{on})v_{in}$$

$$(4) v_A = -(R_{M3} || r_{on})g_{mn}v_{in} \approx -\frac{g_{mn}}{g_{mp}}v_{in}$$

$$(5) v_{out} = -R_{out}g_{mp}v_A = R_{out}g_{mp}\frac{g_{mn}}{g_{mp}}v_{in} = g_{mn}(r_{op} || r_{on})v_{in}$$

$$(6) v_{out1} = g_{mn}(r_{op} || r_{on})v_{in1}, \quad v_{out2} = -g_{mn}(r_{op} || r_{on})v_{in2}, \quad v_{out} = v_{out1} + v_{out2} =$$

$$g_{mn}(r_{op} || r_{on})(v_{in1} - v_{in2}) \rightarrow A_{v,diff} = \frac{v_{out}}{v_{in1} - v_{in2}} = g_{mn}(r_{op} || r_{on})$$

$$(7) A_{v,com} = 0$$

第 9 章

□ 1

$$(1) \text{Loop gain: } \beta A = 100, \text{ Close loop gain: } \frac{A}{1+\beta A} = \frac{1000}{1+100} = \underline{9.9}$$

$$(2) R_{out} = R_{amp} \frac{1}{1+\beta A} = \underline{9.9\Omega}$$

$$(3) BW_{FB} = BW_{amp}(1 + \beta A) = \underline{101kHz}$$

$$(4) GB_{amp} = 1MHz, GB_{FB} = 9.9 * 101kHz = 1MHz$$

第 10 章

$$(1) \omega_{p2} \geq 2\beta\omega_u = 200kHz$$

$$(2) \omega_{p2} \geq 4\beta\omega_u = 400kHz$$

第 11 章

□ 1

$$V_{in,min} = V_{OD,SS} + V_{GS1} = \underline{1.2V}$$

$$V_{in,max} = V_{DD} - (|V_{OD3}| + |V_{TH3}|) + V_{TH1} = \underline{V_{DD} - 0.2V}$$

□ 2

$$V_{in,min,com} = V_{OD,SS} + V_{GS1} = \underline{1.2V}$$

$$V_{in,max,com} = V_{DD} - (|V_{OD3}| + |V_{TH3}|) + V_{TH1} = \underline{V_{DD} - 0.2V}$$

□ 3

$$V_{in,min} = V_{OD,SS} + V_{GS1} = 2V_{OD} + V_{TH}$$

$$V_{in,max} = V_X - V_{OD1} + V_{GS1} = (V_{b1} - V_{GS3}) - V_{OD1} + V_{GS1} = V_{b1} - V_{OD}$$

$$V_{out,min} = V_{b2} - V_{TH5} = V_{b2} - V_{TH}$$

$$V_{out,max} = V_{b3} + |V_{TH7}| = V_{b3} + V_{TH}$$

□ 4

$$V_{in,min} = V_{OD1} + V_{TH1} + V_{OD9} = V_{TH} + 2V_{OD}$$

$$V_{in,max} = V_{DD} - |V_{OD,SS}| - |V_{GS1}| = V_{DD} - 2V_{OD} - V_{TH}$$

$$V_{out,min} = V_{b1} - V_{TH3} = V_{b1} - V_{TH}$$

$$V_{out,max} = V_{b2} + |V_{TH5}| = V_{b2} + V_{TH}$$

□ 5

図 1.1.1

初段 $V_{in,min} = 2V_{OD} + V_{TH}$, $V_{in,max} = V_{DD} - V_{OD} + V_{TH}$, $V_{out,min} = 2V_{OD}$, $V_{out,max} = V_{DD} - V_{OD}$

二段目 $V_{in,min} = V_{OD} - V_{TH}$, $V_{in,max} = V_{DD} - V_{TH} - V_{OD}$, $V_{out,min} = V_{OD}$, $V_{out,max} = V_{DD} - V_{OD}$

図 1.1.2

初段 $V_{in,min} = 2V_{OD} + V_{TH}$, $V_{in,max} = V_{b1} - V_{OD}$, $V_{out,min} = V_{b1} - V_{TH}$, $V_{out,max} = V_{b2} + V_{TH}$

二段目 $V_{in,min} = V_{OD} - V_{TH}$, $V_{in,max} = V_{DD} - V_{TH} - V_{OD}$, $V_{out,min} = V_{OD}$, $V_{out,max} = V_{DD} - V_{OD}$

第 1.2 章

□ 1

補償前

$$\omega_{AB} \approx \frac{1}{\frac{1}{2}C_L r_o}, \quad \omega_{XY} \approx \frac{1}{2C_{SD} \frac{1}{g_m}}, \quad \omega_{EF} \approx \frac{1}{(2C_{SD} + C_G) g_m r_o^2}$$

補償後：2段なので、補償の容量は E-A 間、F-B 間につける $\rightarrow C_{cEF} = \frac{g_{m,9,10} r_{o,9,10}}{2} C_c$,

$$C_{cAB} = C_c$$

$$\omega_{AB} \approx \frac{1}{\frac{1}{2}(C_L + C_C) r_o}, \quad \omega_{XY} \approx \frac{1}{2C_{SD} \frac{1}{g_m}}, \quad \omega_{EF} \approx \frac{1}{\left(2C_{SD} + C_C + \frac{g_m r_o}{2} C_C\right) g_m r_o^2} \approx \frac{1}{\frac{g_m^2 r_o^3 C_C}{2}}$$

よって、もともと接近していた ω_{AB} , ω_{EF} のうち、 ω_{EF} が大幅に低い周波数となることで、極が分離し、安定化する